



The 22nd Offshore Symposium

Redefining Offshore Development: Technologies and Solutions

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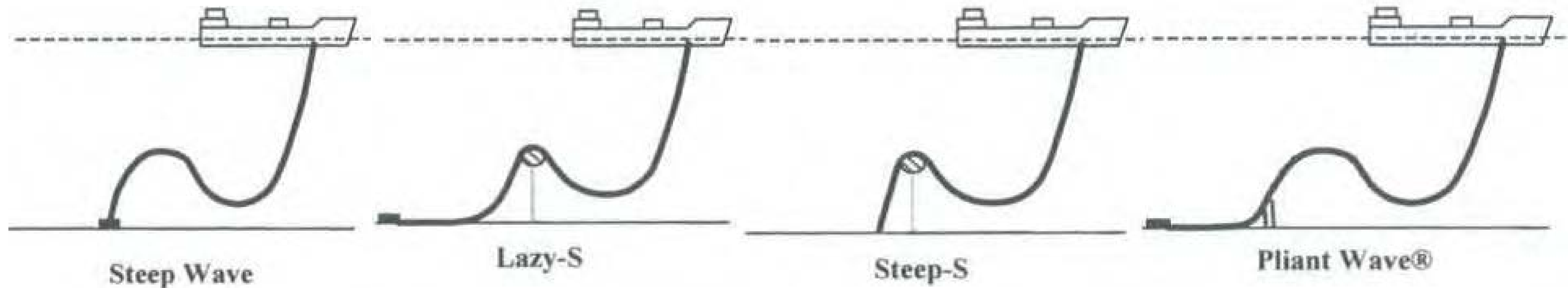
Revisiting Global Response of FPSOs in Shallow Water and the Riser Analysis Requirements

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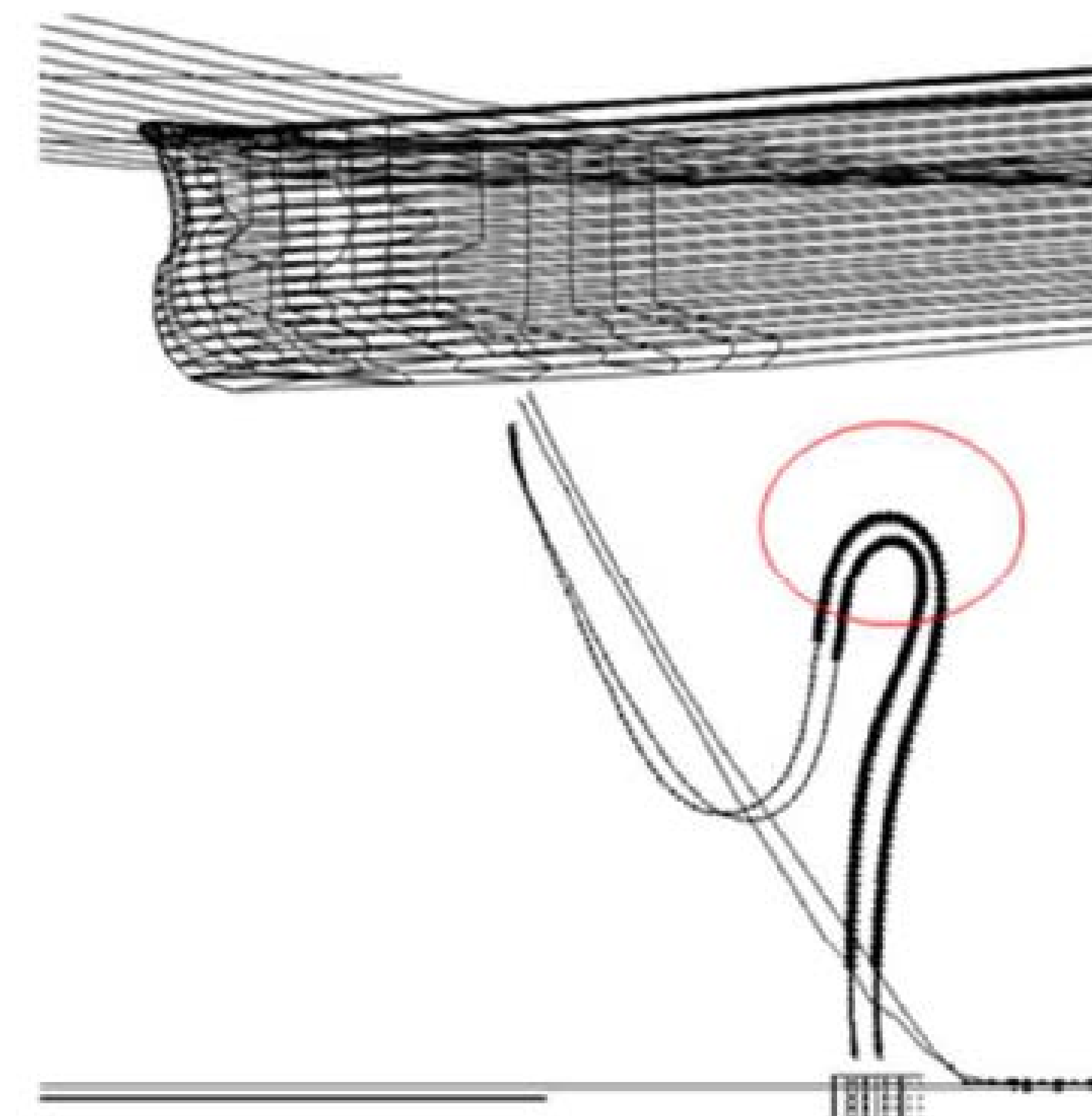
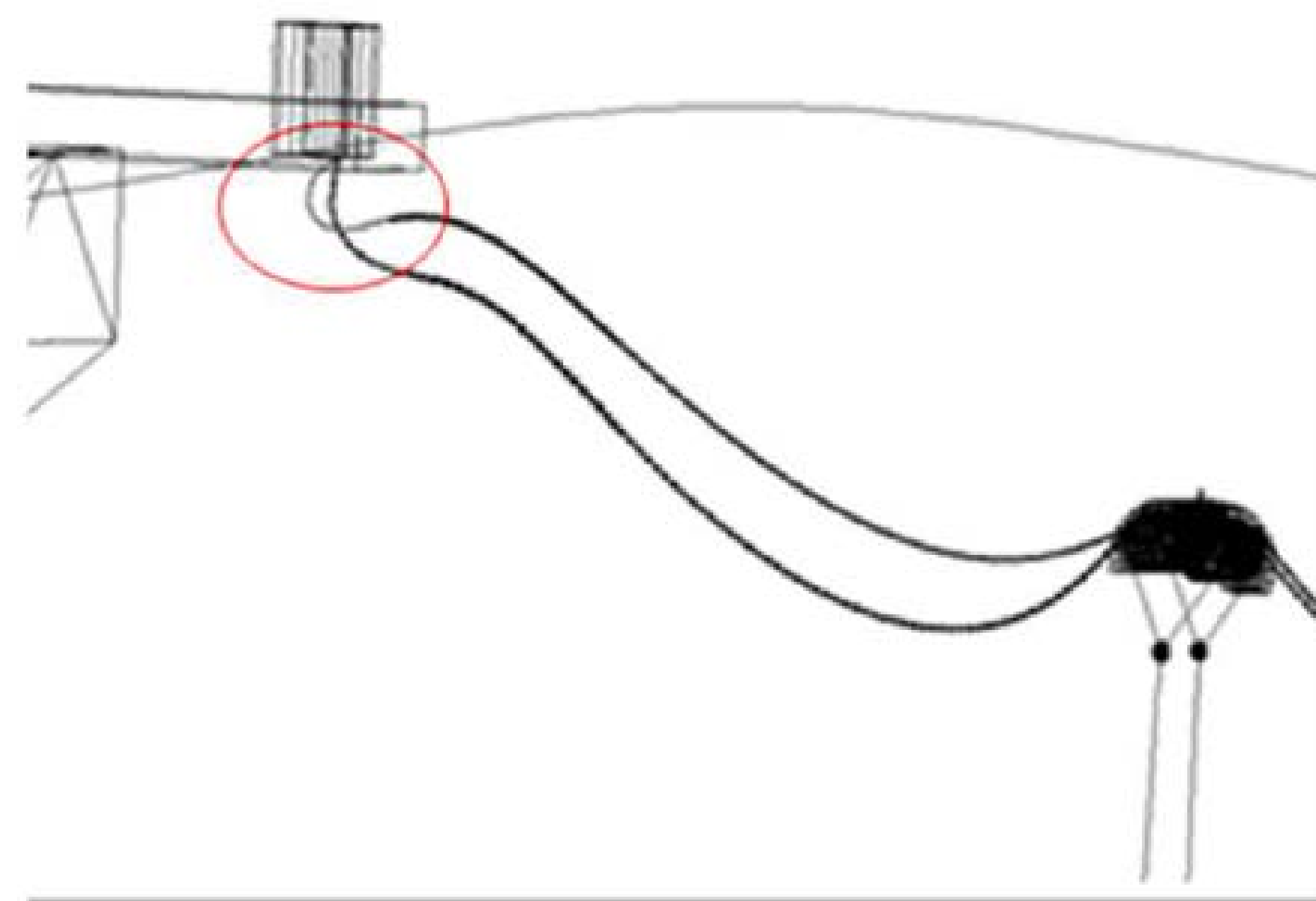
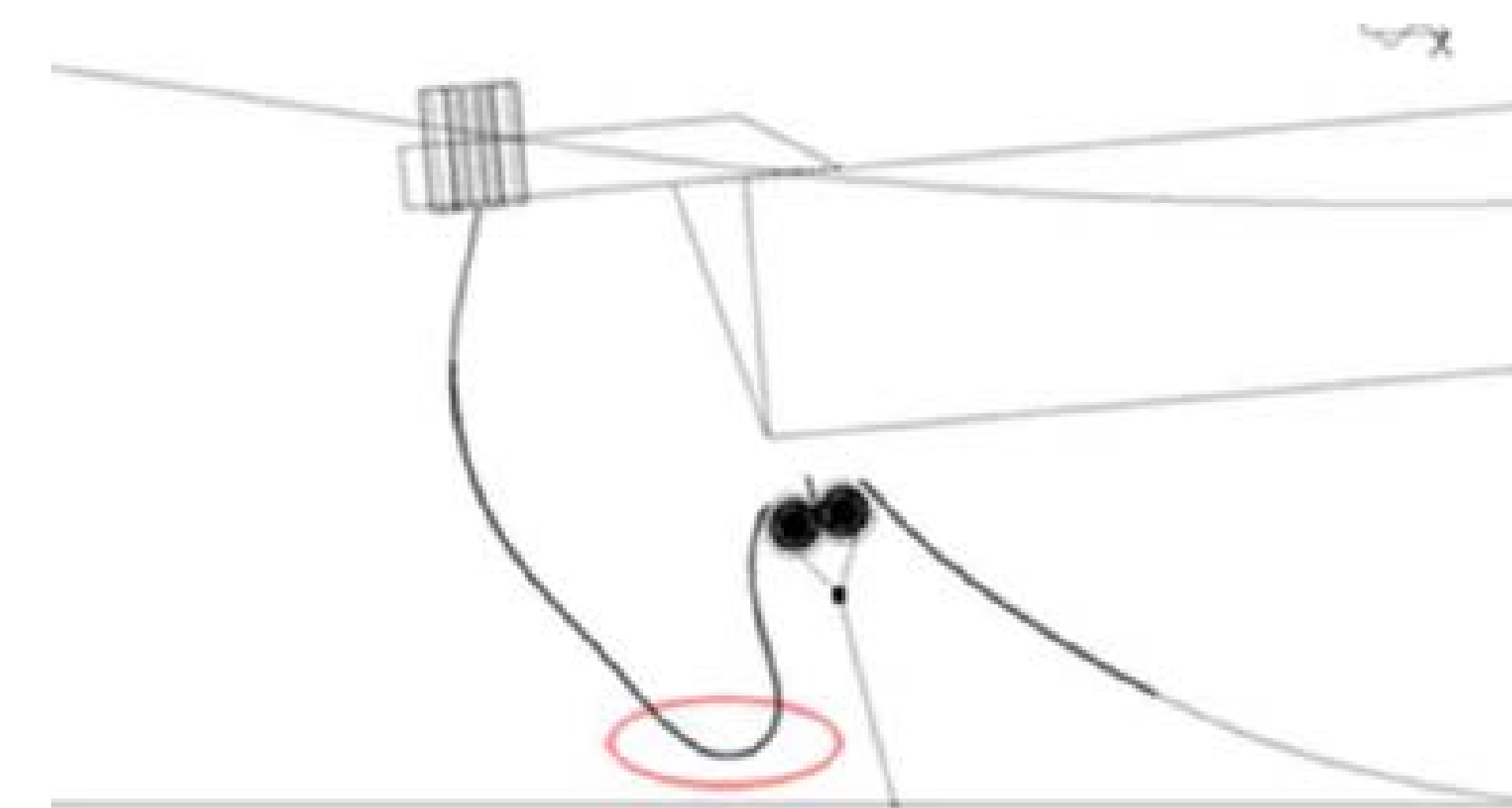
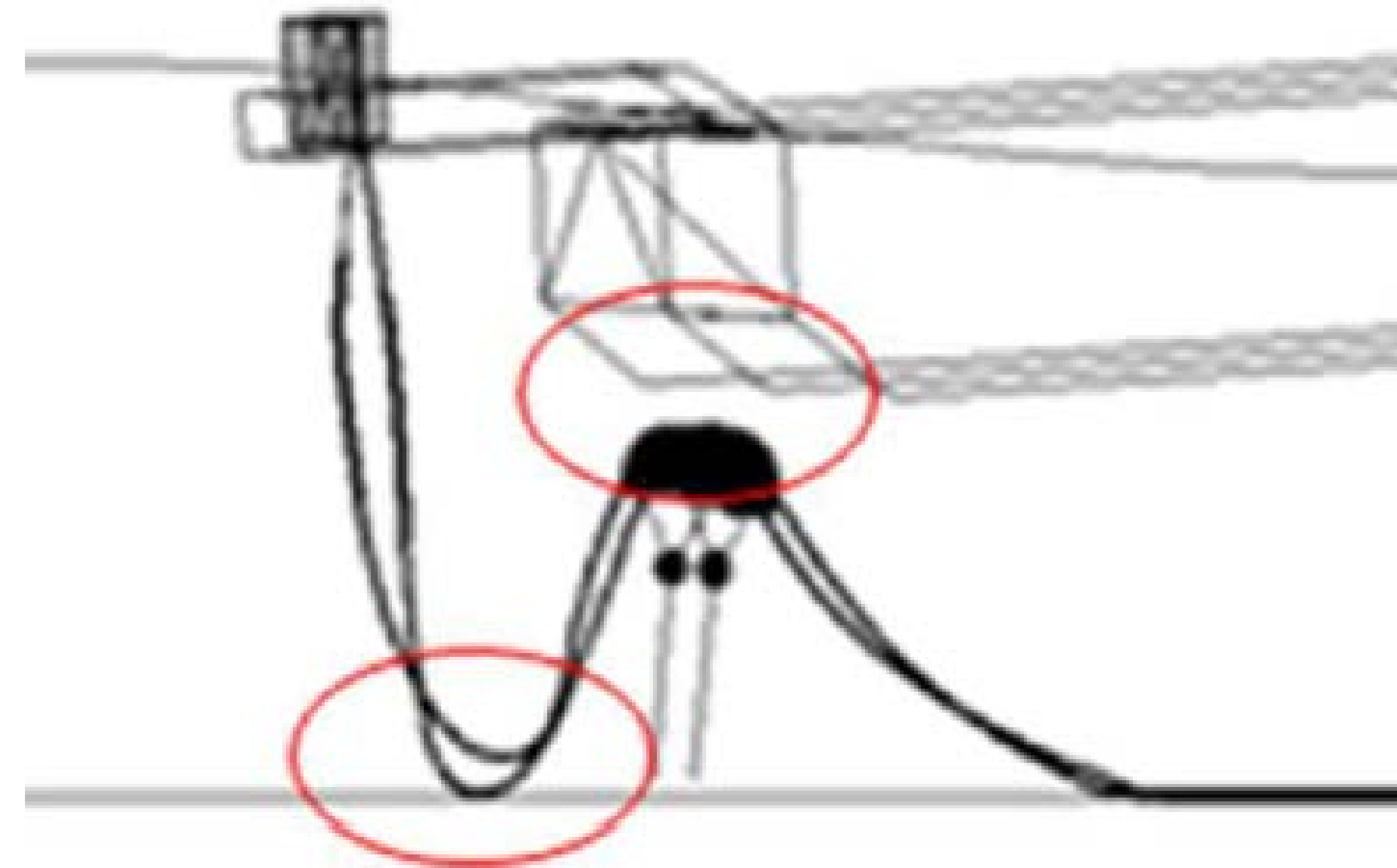
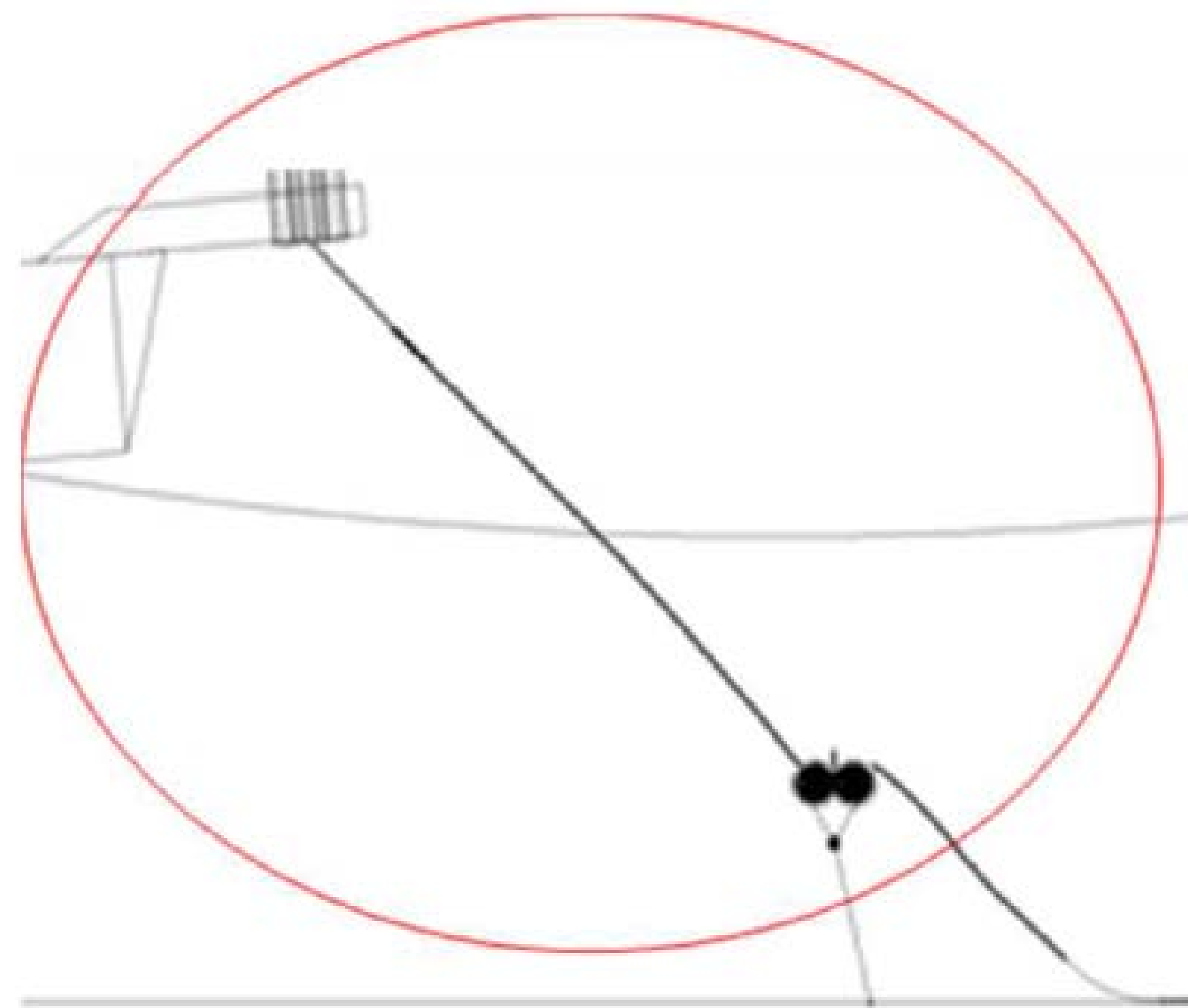


Motivations



- Highly nonlinear mooring system response in shallow water systems ($WD < 150\text{m}$)
- Complex nature of shallow water hydrodynamics
- Water depth limitations
- Proximity of risers with other structures (vessel, mooring lines, other structures)

Motivations



Ref: AOG • Innovative Riser Configurations for Shallow Water • Claus Dencker Christensen • Emad Libis

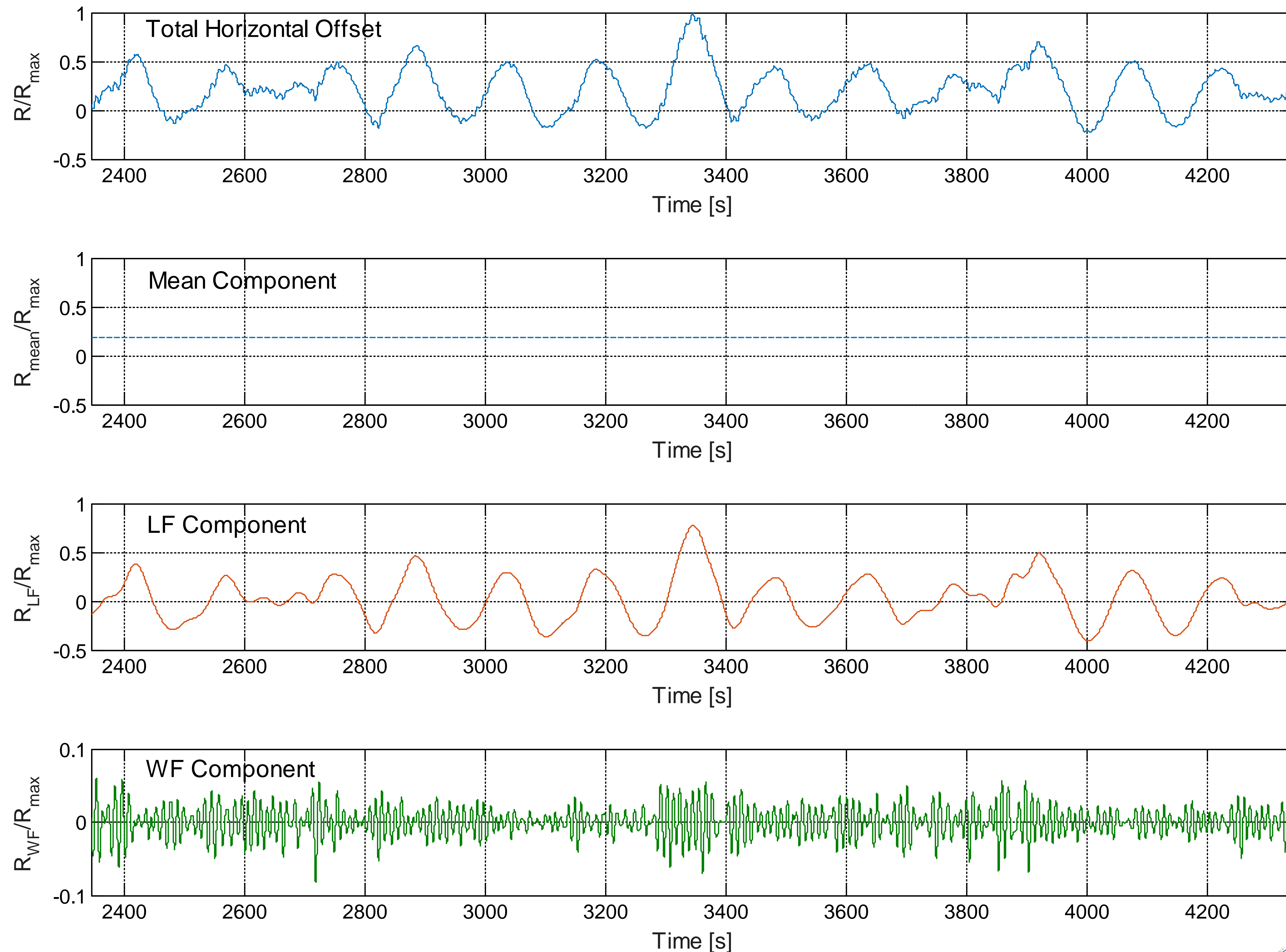
Motivations

- Complex nature of the problem + Conservative Assumptions:
 - Complex riser configurations (e.g. restricted S)
 - Heavier riser structures
 - Added ballast
 - Added stiffness layers
 - Cost

Presentation Structure

- Global Response of FPSOs in Shallow Water
 - Focus on horizontal offset
- Application of Global Responses in Riser Analysis
 - Uncoupled Riser Analysis
- Case Study
 - Global Response of mooring system
 - Statistical Analysis of Extreme Offset and Extreme Wave Height
- Concluding Remarks

Global Response of FPSOs in Shallow Water



Riser Analysis

► Coupled Riser Analysis

- Modeling mooring legs/risers/vessel and their contribution to the response
- Simulation considers vessel LF and WF responses (simultaneously)
- Irregular wave analysis for 3hr duration (multiple seeds)
- Usually done for global analysis purposes
- Difficult to model all the riser details (and the devil is in the details)
- Limited to few critical cases

Riser Analysis

- ▶ Uncoupled Riser Analysis
 - The vessel is placed at a “representative” extreme LF offset
 - Vessel WF response is captured by vessel motion RAOs
 - Regular wave analysis or Irregular wave analysis of a short duration (~200-300sec)
 - Model includes all riser details
 - Suitable for large analysis matrix

Riser Analysis

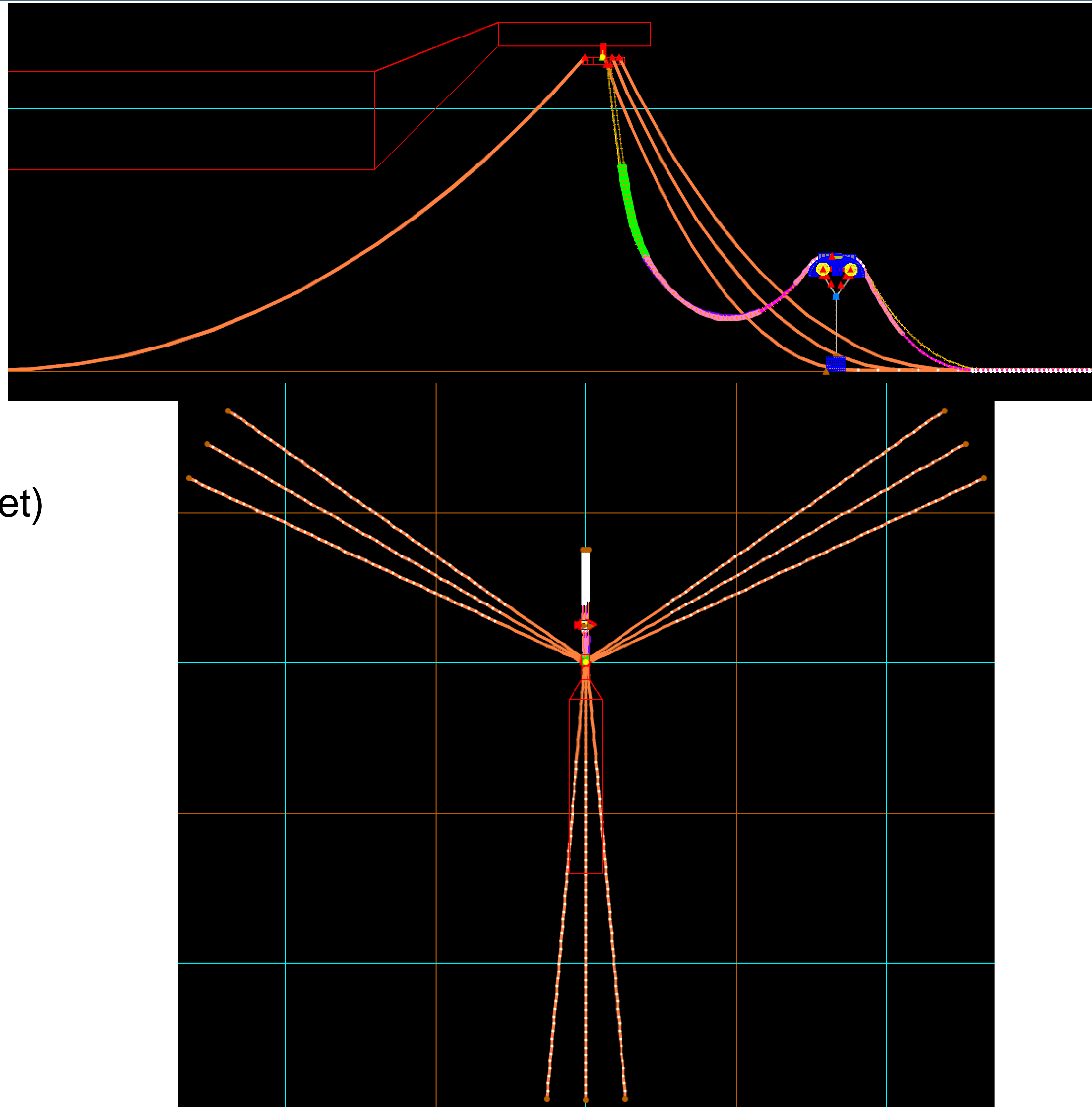
► Challenge (problem definition)

- New codes rely heavily on coupled riser analysis
 - Not used very frequently in actual design process
- The “representative” extreme LF offset to be used for uncoupled analysis is not clearly defined in riser codes
 - Some texts in previous rev of codes and standards are removed (e.g. API RP 17-B)
- Some requirements have been adopted from deepwater systems
- Mooring codes definition of total design offset (Frequency Domain)
 - **Design Offset** = $\max [\text{Mean Offset} + \text{MPM (LF Offset)} + \text{Significant (WF Offset)}, \text{Mean Offset} + \text{Significant (LF Offset)} + \text{MPM (WF Offset)}]$
- Conservative solution used in riser analysis:
 - **MPM Quasi-Static Offset happens with Hmax**

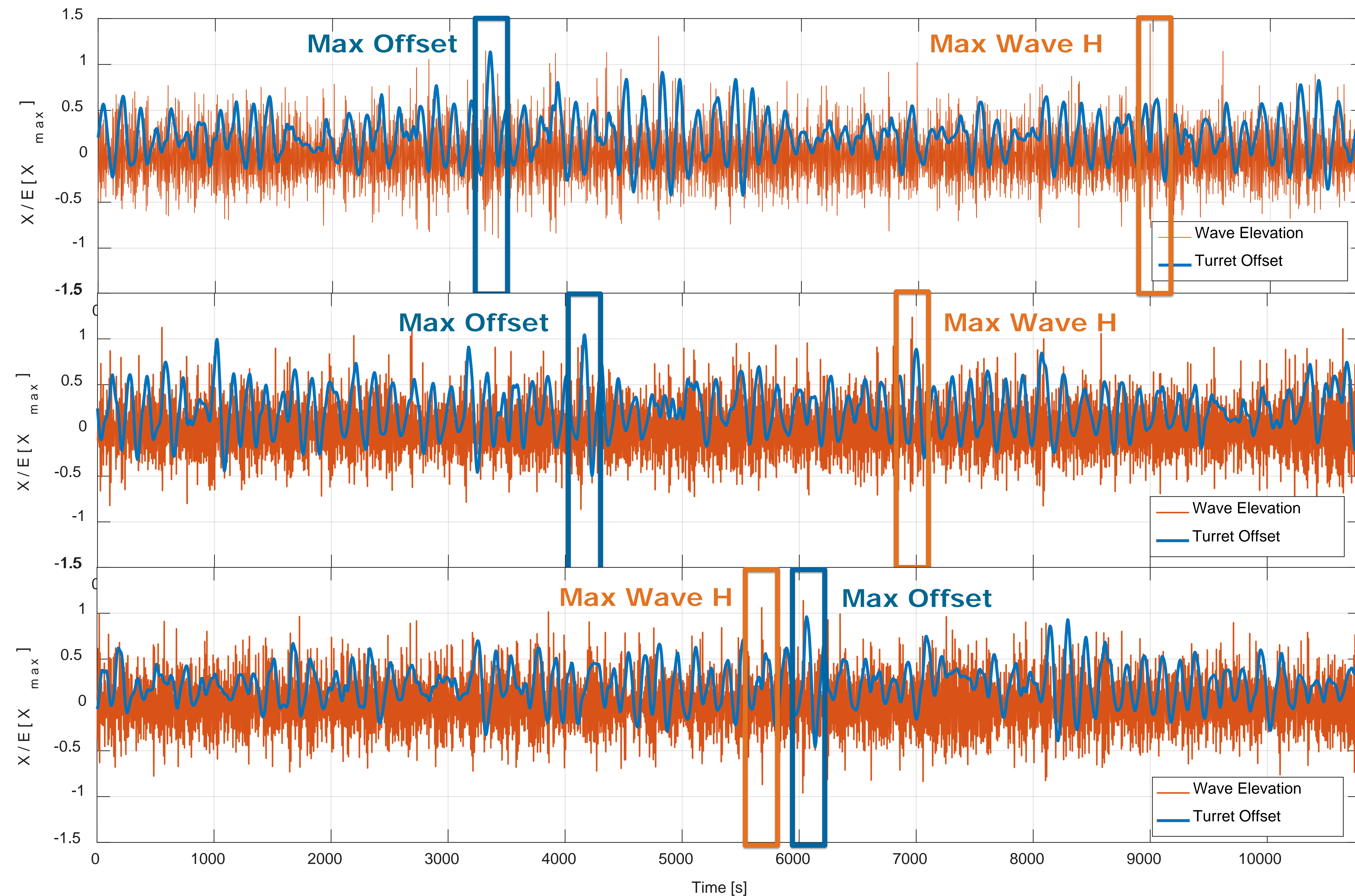
Case Study

Water Depth: ~ 60m
Mooring System: External Turret
Anchor Legs: 3 legs in 3 groups (all chain)
Vessel: Aframax size (small topside)
100yr Hs: ~ 7.0m
Riser: Lazy S (midwater arch)

Model test and Numerical Simulation:
Environment: 100yr Design case (critical offset)
Seeds: 5 random seeds (3hr each)

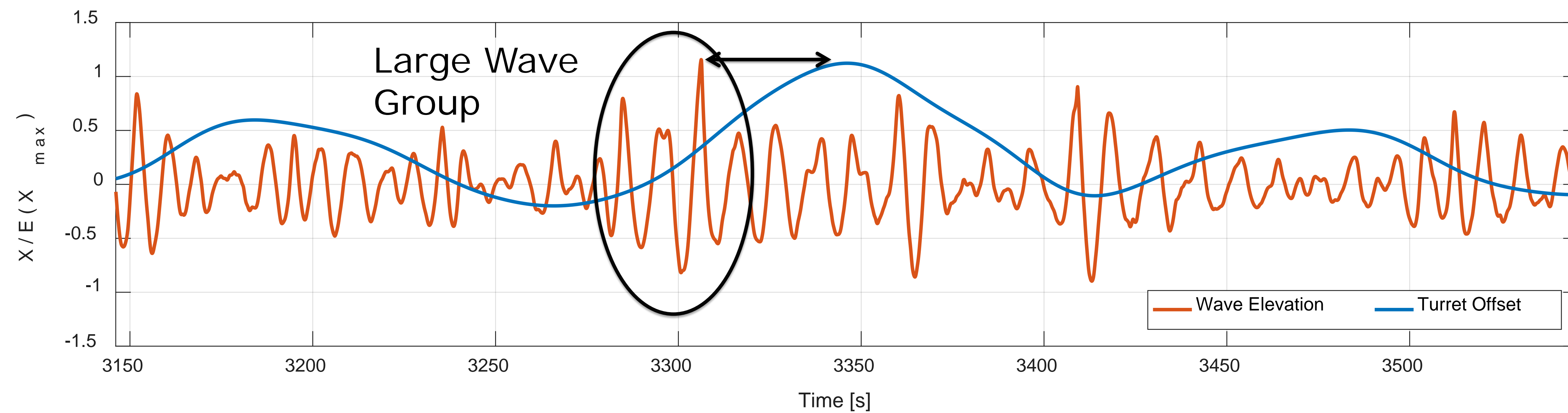


Global Response of the Mooring System

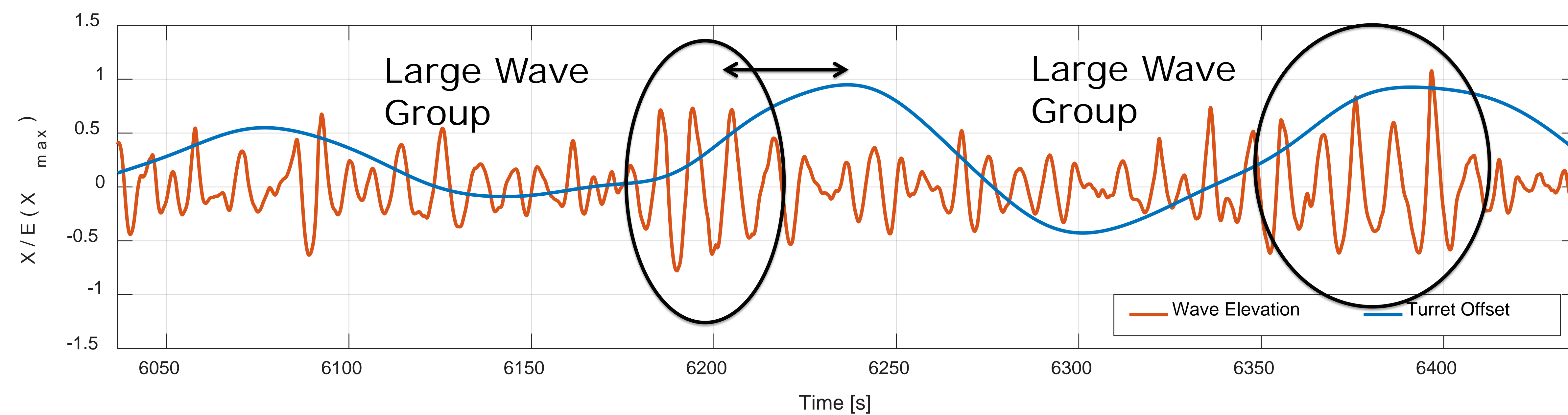


Global Response of the Mooring System

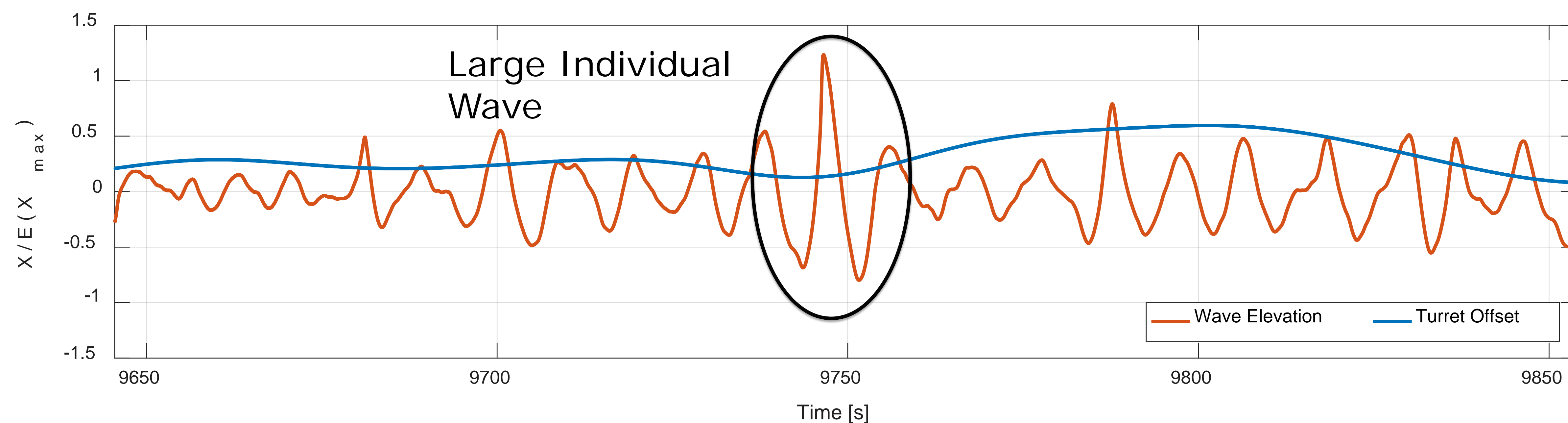
Example 1:
Max Offset



Example 2:
Max Offset



Example 3:
Max Wave H

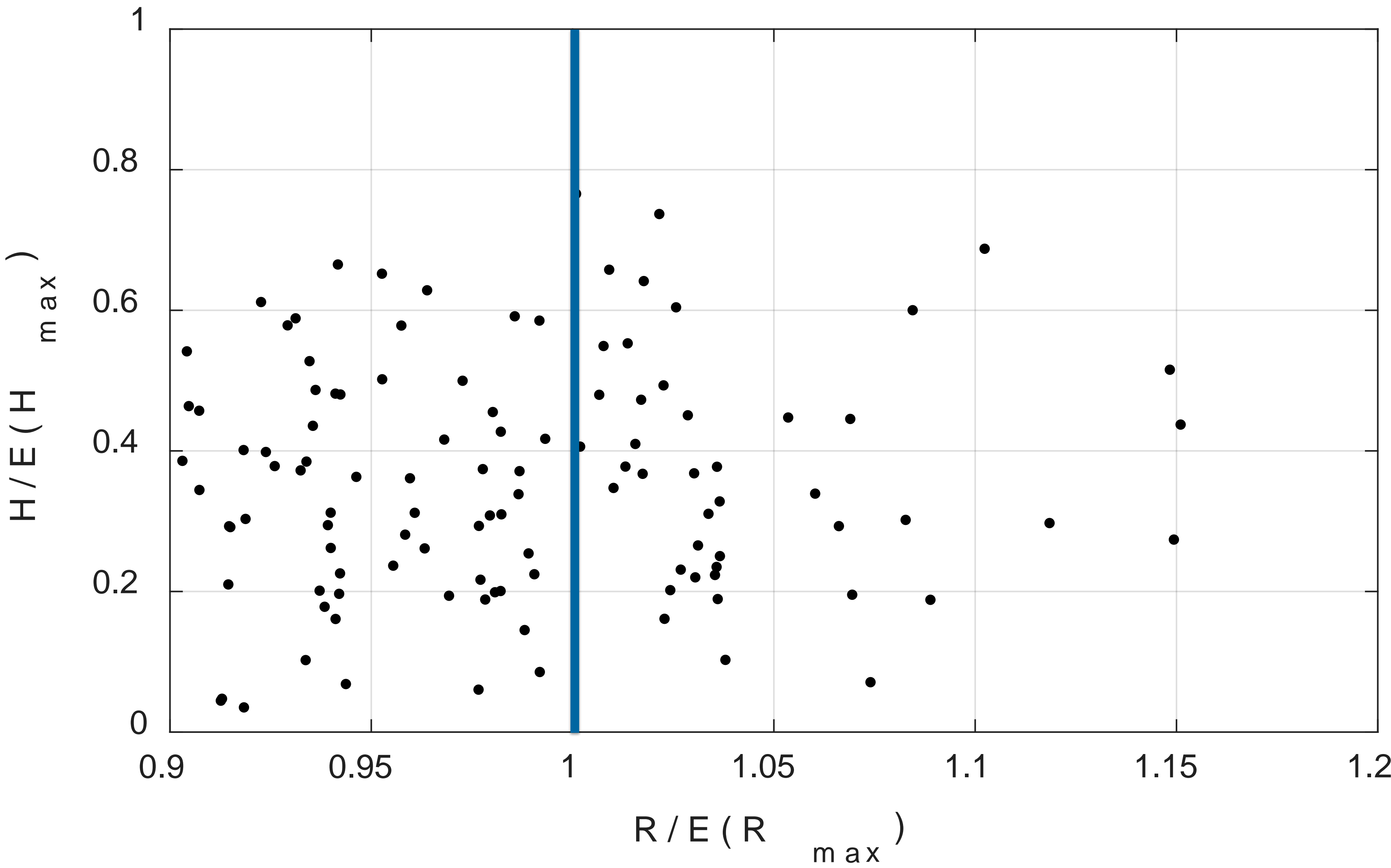


Statistical Analysis of Extreme Offset and Extreme Wave Height

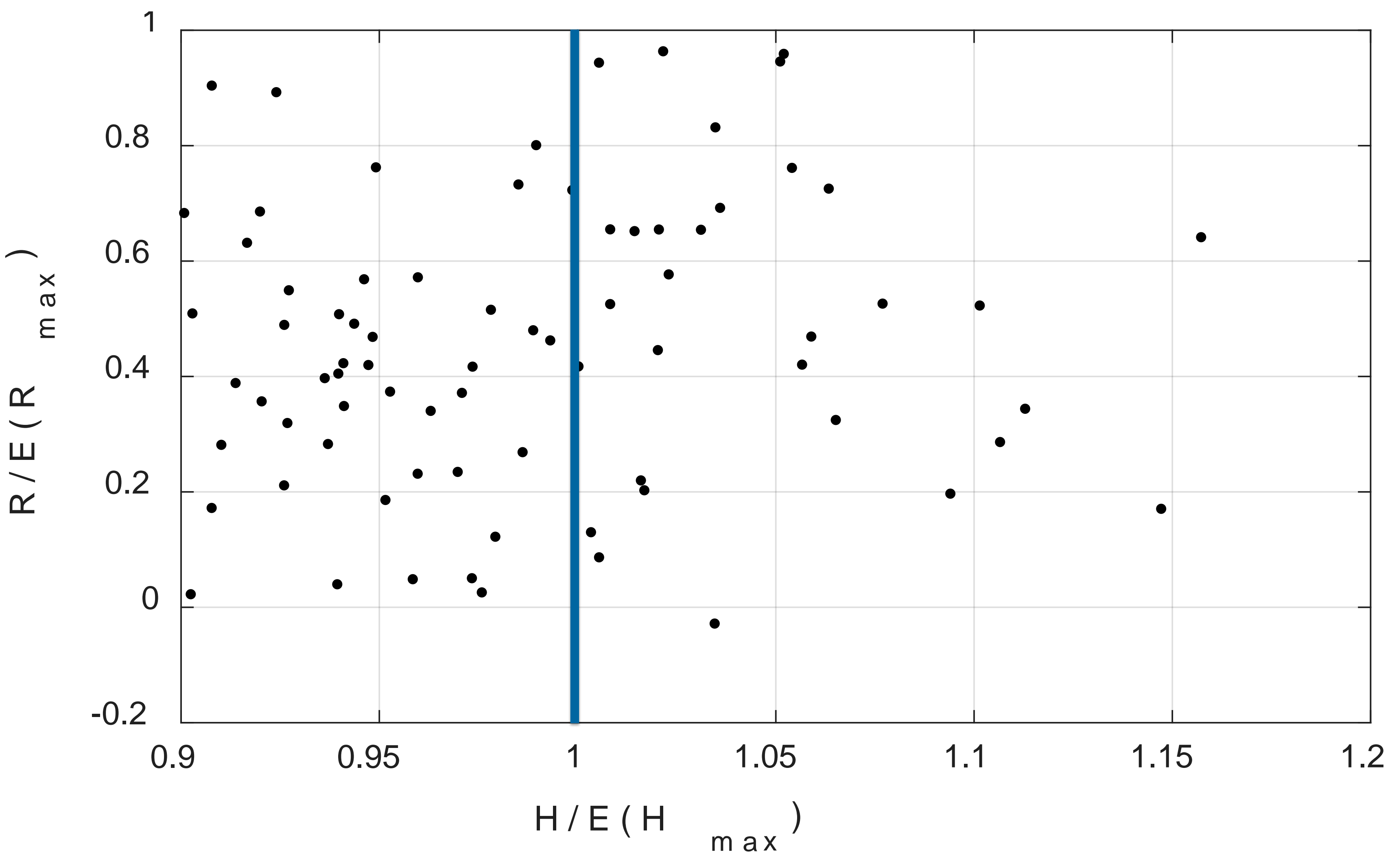
- ▶ Time domain simulations
 - Same system with same initial setup
 - Model verified with model test results
 - 50 seeds (3 hr each)
 - Same environmental condition as the model test

Statistical Analysis of Extreme Offset and Extreme Wave Height

Maximum Offset and Associated Wave Height



Maximum Wave Height and Associated Offset



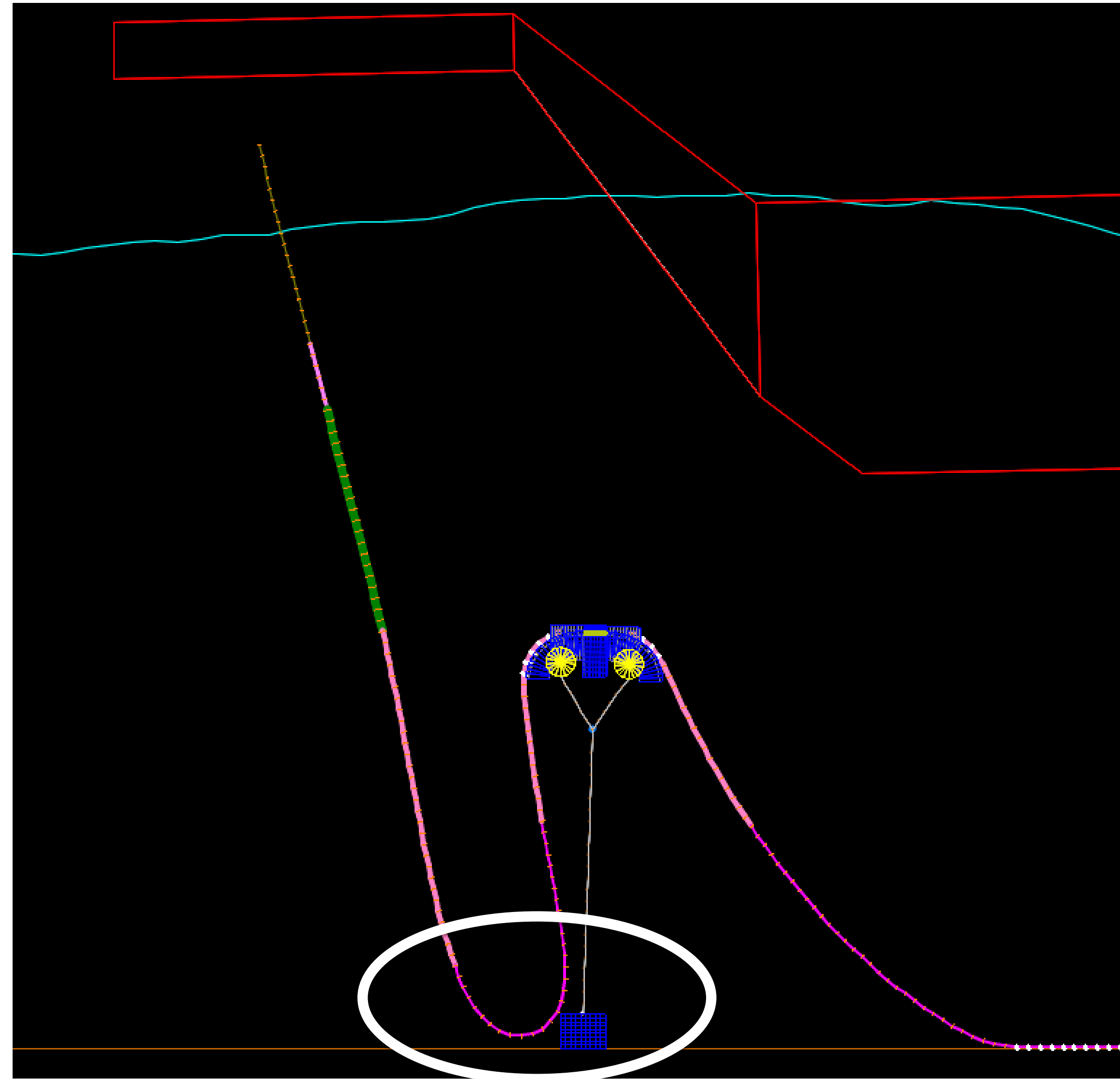
At Maximum Offset	Average of Associated Wave Height	
	$E(H) / E(H_{max})$	$E(H) / H_s$
	0.36	0.65

At Maximum Wave Height	Average of Associated Offset	
	$E(R) / E(R_{max})$	$E(R) / R_s$
	0.48	0.62

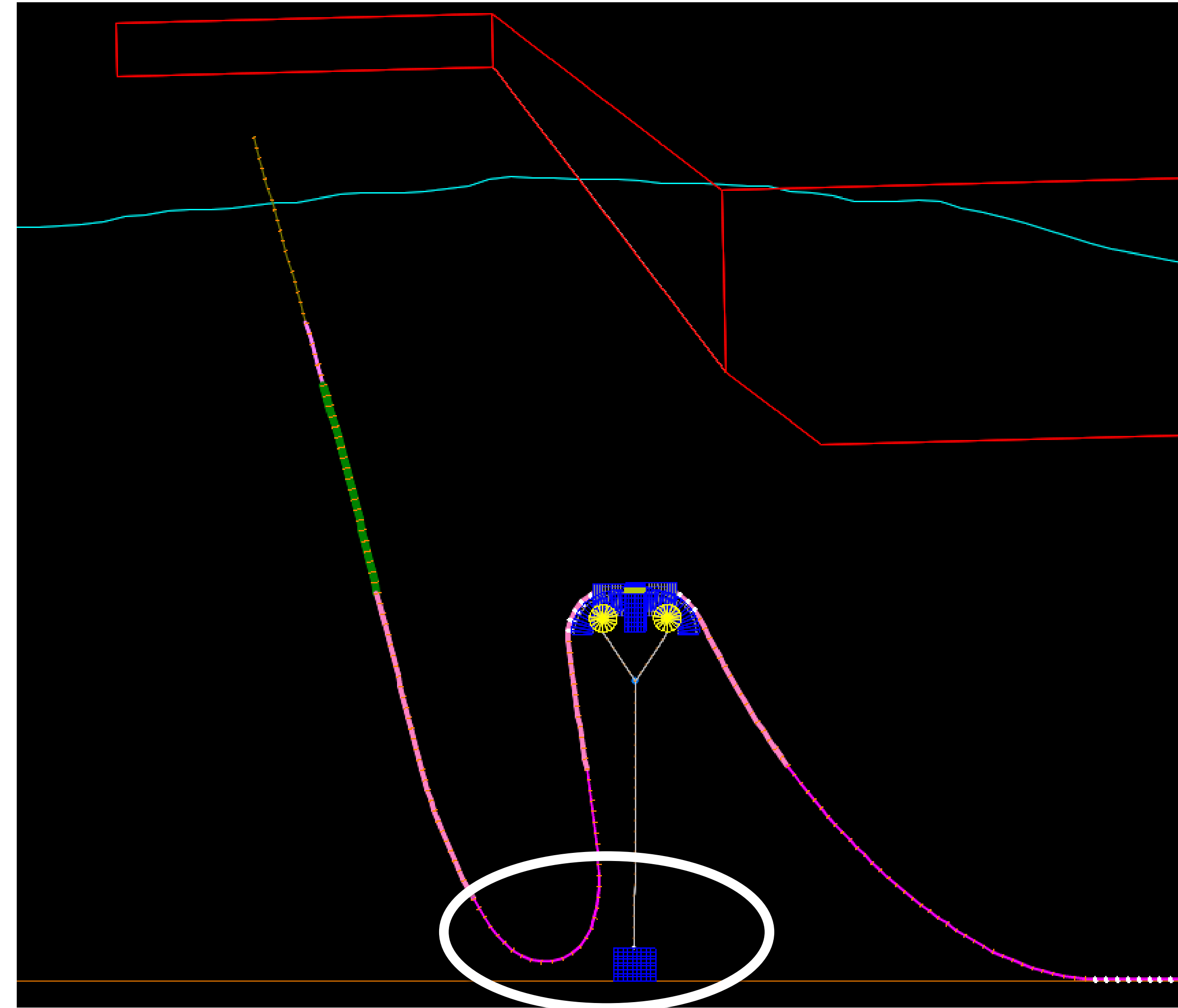
Concluding Remarks

- The comments made here are based on one example. However, based on our experience they can be extended to other systems.
- Maximum wave height and maximum quasi-static offset are not correlated and they do not coincide.
- The natural vessel response causes a gap between the large individual wave in the group and the large corresponding offset. The gap depends on the vessel response.
- The assumption used in riser design that MPM quasi-static offset and Max wave height coincide is very conservative.
- An approach similar to that used in mooring design (Max Offset + Sig Wave, Sig Offset + Max H) seems to be more representative and is recommended for uncoupled analysis purposes.

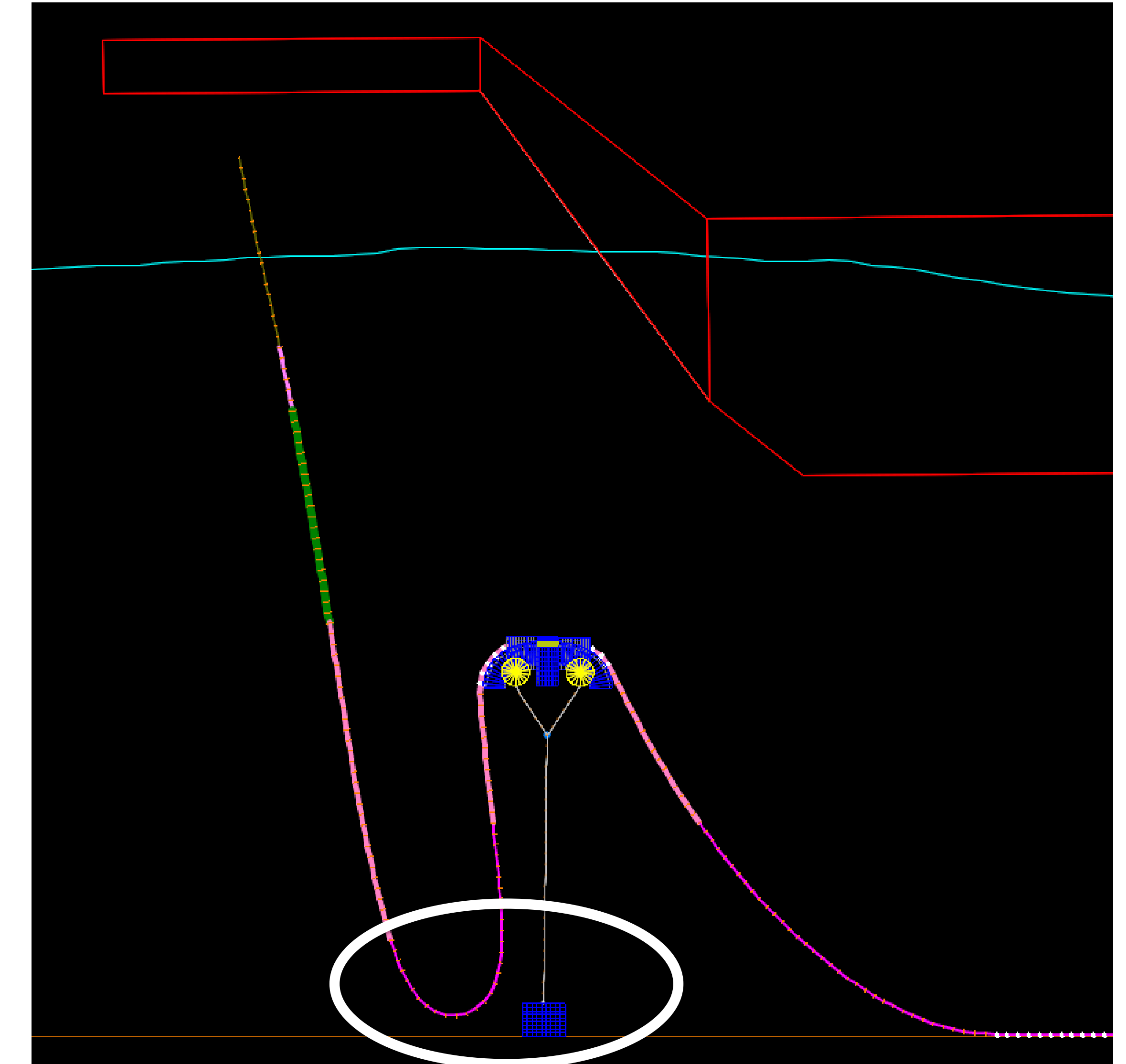
Concluding Remarks



MPM Offset + Hmax



Sig Offset + Hmax



MPM Offset + Hs